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**A STUDY ON LAYOUT AND GROWTH
ASSOCIATED WITH MICROSTRIP RANGE
ANTENNA WITH REGARD TO VAST DUAL
BAND OPERATION**

A Study on Layout and Growth Associated With Microstrip Range Antenna With Regard To Vast Dual Band Operation

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Abstract – This paper presents a novel plan of space stacked two components rectangular microstrip exhibit antenna (SRMAA) for triple band operation. Assuming that the ground plane of SRMAA is minimized to 48.8% by uprooting the copper layer on either side of vertical hub of the substrate from the middle, believers triple-band into double groups. Further, by lessening the ground plane to 76.8%, the antenna improves impedance transfer speed of every working band in the double band operation and gives greatest 40.1% and 50% of impedance data transmission and upgrades the increase from 2.07 to 3.73db without adapting much the way of omni directional radiation attributes. The proposed antennas are basic in their geometry and are created utilizing ease glass epoxy substrate material. These antennas may find provisions for the microwave correspondence frameworks working at IEEE 802.11a (5.15 - 5.35GHz), HIPERLAN/2 (5.725 -5.825GHz) and X (8 -12.5GHz) band of frequencies.

INTRODUCTION

As of late, the utilization and impressive investment in microstrip antennas (MSAs) has come to be broad in view of its huge benefits of little size, light weight, flat profile, minimal effort and run integrability with microwave circuits. Then again, one of the genuine restrictions of MSAs is their thin impedance data transfer capacity and easier addition. Numerous guaranteeing procedures are accessible in the writing for the upgrade of impedance transfer speed and addition, for example utilization of stacked setup , extra resonator , opening coupling , parasitic patch , and so forth. However these strategies require thick substrate and likewise increment the territory of the antenna.

Further, double or triple band antennas have picked up wide consideration in numerous microwave conveyance frameworks on the grounds that they dodge the utilization of divide antennas for transmit/receive provisions for every working band, especially in manufactured opening radar (SAR) . Different systems are accessible in the writing to accomplish double band operation . In this study, a modest space stacked exhibit strategy has been utilized to accomplish triple band operation. To change over triple band into double band, the ground plane is minimized. The improvement of impedance transmission capacity at every working band and increase is accomplished by utilizing ideal ground plane of the cluster design without updating the way of radiation attributes. This sort of study is infrequently discovered in the literary works.

EXPLANATION REGARDING ANTENNA GEOMETRY

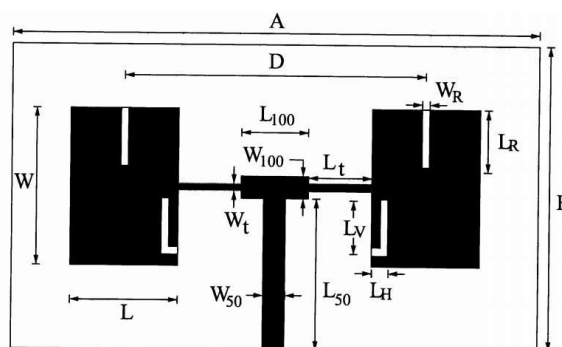


Figure : Geometry of SRMAA

The proposed antennas are designed using low cost glass epoxy substrate material of thickness $h = 0.16$ cm, permittivity $\epsilon_r = 4.2$ and area = $A \times B$. The artwork of the suggested antennas is portrayed utilizing workstation programming Auto-CAD 2006 to attain better precision. The antennas are created utilizing photolithography process.

Figure shows the top view geometry of space stacked two component rectangular microstrip cluster antenna (SRMAA). The length L and width W of the patch is intended for full recurrence of 5GHz, utilizing the comparisons accessible within the expositive expression for outline of rectangular fix . The rectangular spaces are put at the core along the length L of upper non emanating edge of the patch. The half U formed spaces are put inside the patch

from bottom non transmitting edge L at a separation of 1mm. The measurements of spaces are taken as far as λ_0 , where λ_0 is free space wavelength in cm. The length Lr and width WR of rectangular space is taken as $\lambda_0/8.57$ and $\lambda_0/60$ individually. The sizes of half U molded space having flat length L_H and vertical length L_V are taken as $\lambda_0/30$ and $\lambda_0/8$ individually. The separation D between the two transmitting components from their focal point ouGht to be $\lambda_0/2$ for least side projections. Anyhow in Fig., D is taken as to keep the food line as minimal as would be prudent for least nourish line misfortune. Further, when D is less than $\lambda_0/2.33$; it comes to be challenging to oblige the food plan between the cluster components. Consequently $D = \lambda_0/2.33$ is treated as ideal in this case. The parallel food plan has wideband exhibition over arrangement nourish and consequently chose hence to energize the exhibit components of Figure. The food course of action demonstrated in Figure is a contact food and has advantage that it might be carved synchronously in addition to antenna components. The parallel food game plan of Figure comprises of a 50Ω microstripline food of length L_{50} and width W_{50} is associated with 100Ω microstripline food of length L_{100} and width W_{100} to structure a two way force divider. A 100Ω quarter wave matching transformer of length L_t and width W_t is joined between 100Ω microstripline nourish and mid purpose of the transmitting components so as to guarantee idealize impedance matching. The lowest part plane of SRMAA is tight ground plane copper shielding. The ground plane shielding of SRMAA is minimized to 48.8% as for ground plane region AxB as indicated in Figure holding its top geometry. This antenna is named as adjusted ground plane space stacked two components rectangular microstrip exhibit antenna (Mrmaa). The measure of copper zone on the ground plane is taken as $A_1 \times B$. Figure shows the lowest part see geometry of extensive adjusted ground plane opening stacked two elements rectangular microstrip array antenna (LRMAA). The size of copper area on the ground plane is taken as $A_2 \times B$ which is 76.8% smaller than the area AxB retaining its top geometry same as that of Figure. The various parameters of proposed antennas are given in Table.

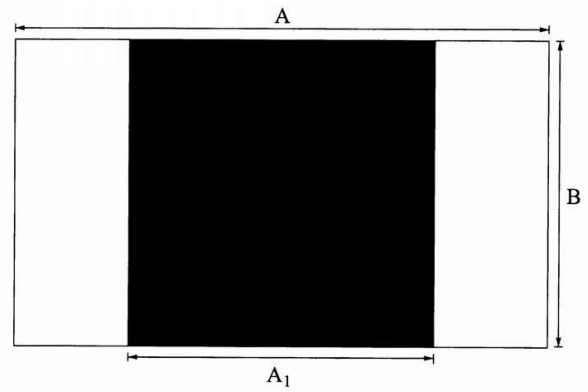


Figure : Ground plane geometry of MRMAA

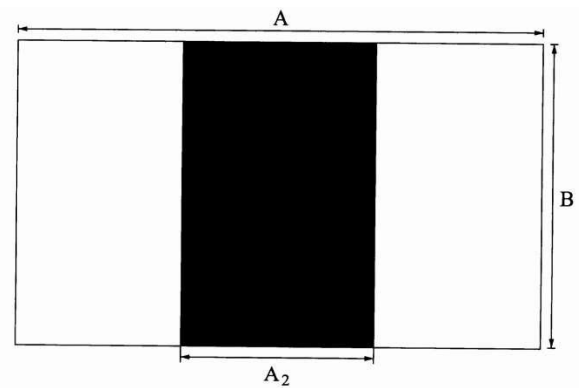


Figure : Ground plane geometry of LRMAA

| Antenna Parameters | Dimensions (cm) | Antenna Parameters | Dimensions (cm) |
|--------------------|-----------------|--------------------|-----------------|
| A | 5.00 | L_{100} | 0.38 |
| B | 3.50 | W_{100} | 0.07 |
| L | 1.41 | D | 2.56 |
| W | 1.86 | A_1 | 2.56 |
| L_t | 0.38 | A_2 | 1.16 |
| W_t | 0.015 | L_R | 0.70 |
| L_{50} | 1.54 | W_R | 0.10 |
| W_{50} | 0.32 | L_H | 0.20 |
| λ_0 | 6.00 | L_V | 0.75 |

Table : Design Parameters of Proposed Antennas

EXPERIMENTAL RESULTS

The impedance transfer speed over return misfortune less than -10db of the proposed antennas is measured on Vector Network Analyzer (Rohde & Schwarz, Germany make Zvk model 1127.8651). The variety of return misfortune versus recurrence of SRMAA is as indicated in Figure. From this figure, it might be seen that, the antenna resounds for three groups of frequencies BW1? BW2 and BW3. the impedance data transfer capacity (BW) at every working band is dead set by utilizing the mathematical statement,

$$BW = \left[\frac{(f_2 - f_1)}{f_c} \right] \times 100 \%$$

Where, f_1 and f_2 are the more level and upper cut-off frequencies of the band individually, when its return misfortune turns into -10db and f_c is the inside recurrence between f_1 and f_2 . The extent of every working band BW_1 , BW_2 and BW_3 in Figure is discovered to be 10.2, 11.7 and 20.64% separately. The triple groups are because of the free reverberation of transmitting components and spaces on SRMAA.

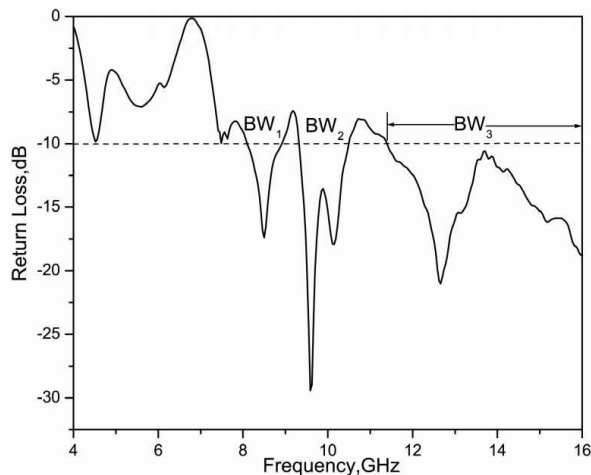


Figure : Variation of return loss verses frequency of SRMAA

The variation of return loss versus frequency of MRMAA is as shown in Figure.

From this graph, it can be observed that, the antenna resonates for dual band of frequencies BW_4 and BW_5 with corresponding magnitudes of impedance bandwidth is 12.1 and 47% respectively. Further, from this figure, it is clear that the two bands BW_1 and BW_2 of Figure merges into a single band BW_4 as shown in Figure. This is due to the impact of diminishment of ground plane in MRMAA. Nonetheless, the data transfer capacity BW_3 demonstrated in Figure improves from 20.64% to 47% i.e. BW_5 which is clear from Figure. Consequently, by altering the ground plane geometry of Srmaa triple band operation could be changed over into double band operation with improved upper band BW_5 . Figure shows the variety of return misfortune versus recurrence of LRMAA. The antenna reverberates again for double groups BW_6 and BW_7 and gives most extreme impedance transmission capacity at every working band i.e. BW_6 and BW_7 . The sizes of impedance transmission capacities of BW_6 and BW_7 are discovered to be 40.1% and 50% individually. These data transmissions are 94.28% and 6.38% more when contrasted with the impedance data transfer capacities BW_4 and BW_5 individually. The upgrade of impedance transmission

capacity of LRMAA is because of the impact of diminished ground plane. This diminished or best ground plane going about as optional space. The surface present around the optional space border increments the electrical length which explain diminish in full recurrence. Consequently the patch and space on the patch reverberates near one another bringing about upgrade of impedance transfer speed .

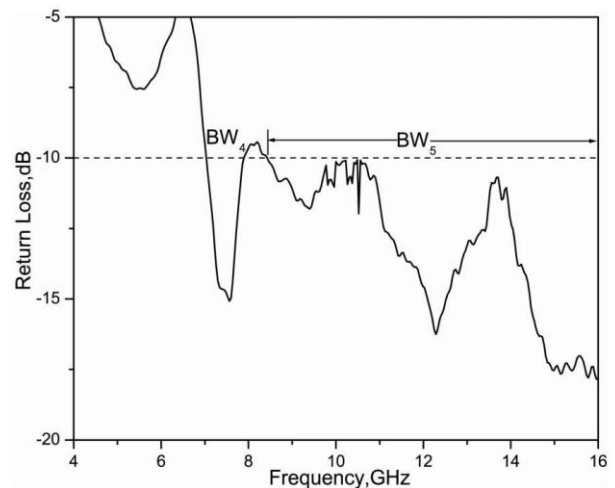


Figure : Variation of return loss verses frequency of MRMAA

The radiation patterns of proposed antennas i.e. antennas under test (AUT) are measured by connecting a standard pyramidal horn antenna in far field region. The AUT is connected in receiving mode and is kept in phase with respect to transmitting pyramidal horn antenna. The power received by AUT is measured from 0° to 360° with steps of 10° . The typical radiation patterns of SRMAA, MRMAA and LRMAA are measured at 8.5, 7.56 and 4.48GHz respectively.

CONCLUSION

From the itemized exploratory study, it is reasoned that triple band operation with omni directional radiation example of antenna is accomplished by outlining Srmaa. By decreasing zone of the ground plane by 48.8% concerning the ground plane region of Srmaa, triple band operation might be changed over into double band operation. Further, if the ground plane region of Srmaa is lessened to 76.8% the most extreme upgrade of impedance transfer speed at every working band in the double band operation is conceivable without much altering the way of omni directional radiation attributes. This method additionally improves the addition from 2.07 to 3.73db. The proposed antennas are straightforward in their configuration, creation and they utilize minimal effort substrate material. These antennas may find applications for microwave communication systems operating at IEEE802.11a

(5.15 - 5.35GHz), HIPERLAN/2 (5.725 - 5.825GHz) and X (8 - 12.5GHz) band of frequencies.

REFERENCES

- Zehforoosh .Y., et. al. (2006), "Antenna design for ultra wide band application using a new multilayer structure", PIERS online, Vol.2, No.6, pp.544-549.
- Kumar .G and Gupta K.C (1984), "Broad-band microstrip antennas using additional resonators gap-coupled to the radiating edges", IEEE Trans Antennas Propag, Vol. 32, No.12, pp.1375-1379.
- Jazi .M.N., et. al. (2008), "Design and implantation of aperture coupled microstrip IFF antenna", PIERS online, Vol.4, No.1, pp.1-5.
- Nishiyama .E. and M. Aikawa (2004), "Wide-band and high gain microstrip antenna with thick parasitic patch substrate", IEEE Antennas and Propag, Soc. Inter. Symp, Vol.1, pp.273-276.
- Wang .W., et. al. (2004), "A dual polarized stacked microstrip antenna sub array for X-band SAR application", IEEE Antennas and Propag, Soc. Inter. Symp, Vol.2, pp.1603-1606.
- Jui Han Lu (1999), "Single feed dual frequency rectangular microstrip antennas with pair of step slots", Electron Lett, Vol.35, No.5, pp.354-355.
- Shun-Yun Lin and Kin-Lu Wong (2001), "A dual frequency microstrip line fed printed slot antennas", Microwave Opt Technol Lett, Vol. 28, No.6, pp.373-375.
- J. Bhal and P. Bhartia (1981), "Microstrip Antennas", Artech House, New Delhi.
- C. A. Balanis (1982), "Antenna Theory Analysis and Design", John Wiley & Sons, New York.
- Wang .H.Y., and Lancaster .M.J (1999), "Aperture-coupled thin film superconducting mender antennas", IEEE Trans Antennas Propag, Vol. 47, No.5, pp.829-836.